



Increasing heat flux



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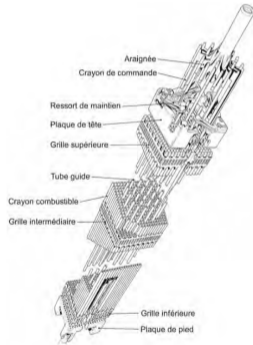


CRITICAL  
HEAT FLUX

## Heating in a nuclear reactor

# Heating in a nuclear reactor

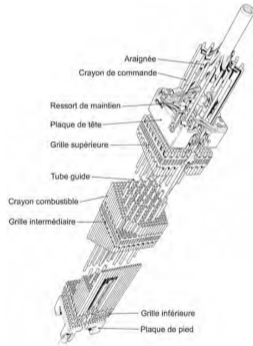
## Complex geometry



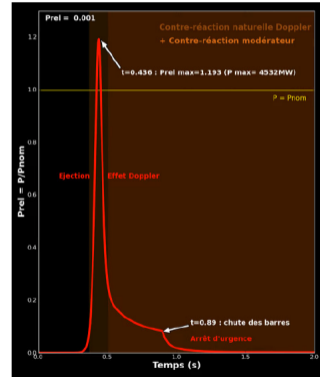


# Heating in a nuclear reactor

## Complex geometry



## Transient power



## Available experiments

Geometry	Stationnary	Transient
Pipe	DEBORA	PATRICIA
Assembly	OMEGA, KATHY	

## Available experiments

Geometry	Stationnary	Transient
Pipe	DEBORA	PATRICIA
Assembly	OMEGA, KATHY	Need code Objective of PhD

# Building a Boiling-Flow Multiphase CFD Framework for Nuclear Reactor Conditions

Journées Écoulements et Fluides de Saclay

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DM2S/STMF/LMEC

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## Ingredients of TrioCMFD

- Numerical framework → TRUST platform
- Conservation equations
- Selection and implementation of closure laws
- Step-by-step validation

## Conservation equations for each phase

Mass conservation :

$$\frac{\partial \alpha_k \rho_k}{\partial t} + \nabla \cdot (\alpha_k \rho_k \vec{u}_k) = \underbrace{\Gamma_k}_{\text{Changement de phase}}$$

Momentum conservation :

$$\alpha_k \rho_k \frac{\partial \vec{u}_k}{\partial t} + \nabla \cdot (\alpha_k \rho_k \vec{u}_k \otimes \vec{u}_k) - \vec{u}_k \nabla \cdot (\alpha_k \rho_k \vec{u}_k) = -\alpha_k \nabla P + \nabla \cdot [\alpha_k \mu_k \nabla \vec{u}_k - \underbrace{\alpha_k \rho_k \overline{u'_i u'_j}}_{\text{Turbulence}}] + \underbrace{\vec{F}_{ki}}_{\text{Forces interfaciales}} + \alpha_k \rho_k \vec{g}$$

Energy conservation :

$$\frac{\partial \alpha_k \rho_k e_k}{\partial t} + \nabla \cdot (\alpha_k \rho_k e_k \vec{u}_k) = -P (\partial_t \alpha_k + \nabla \cdot (\alpha_k \vec{u}_k)) + \nabla \cdot [\alpha_k \lambda_k \nabla T_k - \underbrace{\alpha_k \rho_k \overline{u'_i e'_k}}_{\text{Turbulence}}] + \underbrace{q_{ki}}_{\text{Condensation}} + \underbrace{q_{kw}}_{\text{Chauffage paroi}}$$

Undisputed terms

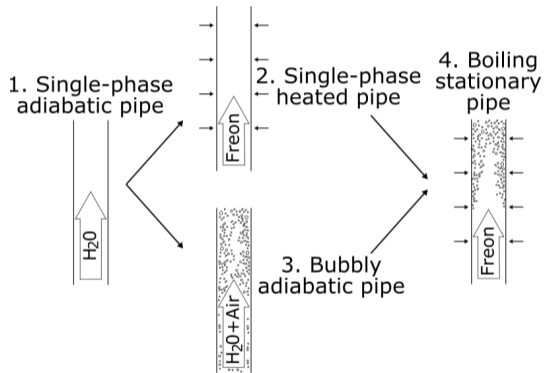
Terms that need to be modeled

## Selected baseline models

Model type	Selected model	Effect
1 $\phi$ turbulence	$k - \omega$	
Adaptive wall law	Reichardt	
	Tomiyama drag	Sets relative velocity
	Sugrue lift	Bubbles sent to wall or core
Interfacial forces	Burns turbulent dispersion	Spreads bubbles
	Lubchenko wall correction	Pushes bubbles from wall
	Constant-coeff virtual mass	Increases bubble inertia
Wall heat flux partition	Kurul-Podowski	Liquid heats or vapor forms ?
Condensation	Zeitoun	

*N.B. : mostly come from experiments on single bubbles at  $P_{atm}$  or from a purely theoretical analysis  $\rightarrow$  Valid in PWR's ?*

## Validation stages

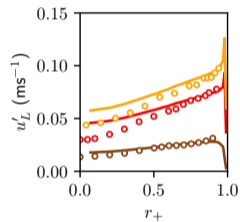
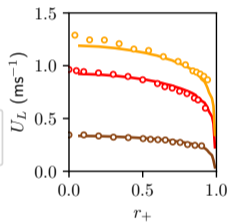
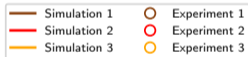


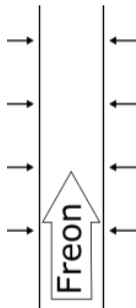




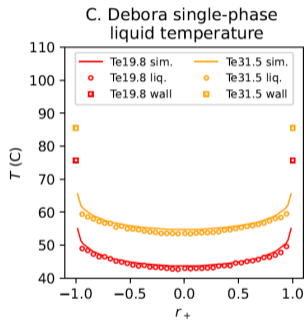
# 1. Single-phase adiabatic pipe flow

Colin et al.  
Single-phase tube





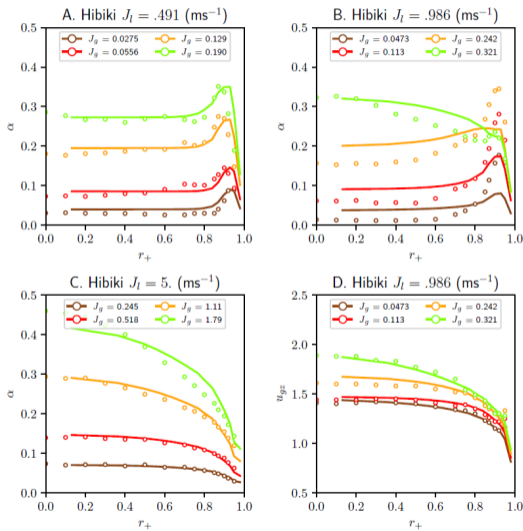
## 2. Single-phase heated pipe flow



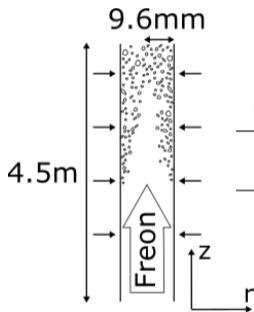


We enforce the experimentally measured bubble diameter

### 3. Bubbly adiabatic pipe flow



## 4. Boiling pipe flow in PWR similarity



DEBORA experiments

Run number	1	2	3
Pressure similarity	Boiling Water Reactor	Pressurized Water Reactor	Pressurized Water Reactor
Liquid velocity	Maintenance ~2m/s	Maintenance ~1m/s	Normal operation ~3m/s

## 4. Boiling pipe flow in PWR similarity

How to close the bubble diameter in boiling flow simulations:

Historical approach:

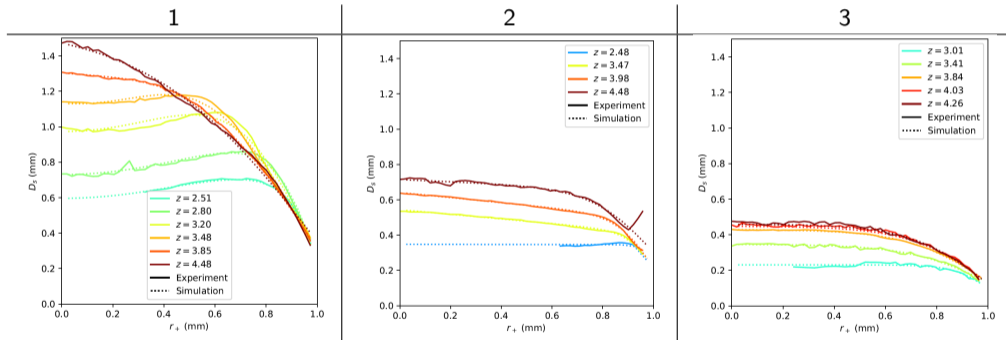
- 1 Build and IATE to predict diameters
- 2 Validate the model on atmospheric-pressure adiabatic stationary flows with momentum closures
- 3 Add boiling and condensation terms

Our approach:

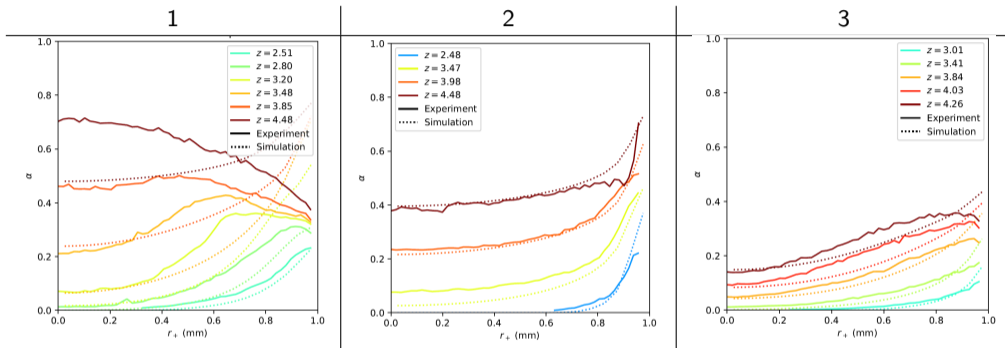
- 1 Select energy and momentum closures
- 2 Enforce 3D map of experimental bubble diameter
- 3 Validate the closures in PWR-similarity conditions
- 4 Future work: model bubble diameters in PWR conditions

## 4. Boiling pipe flow in PWR similarity

### Diameter interpolation



## 4. Boiling pipe flow in PWR similarity



Atmospheric-pressure closure models are not adapted to nuclear reactor-condition boiling flows

For  $u_{\text{bulk}} > 2\text{m/s}$  something pulls the bubbles away from the wall  $\rightarrow$  lift force along  $-\vec{u}_r$

Lack of separate-effect experimental data: still many closure terms to adjust

## 4. Boiling pipe flow in PWR similarity

Choice to concentrate on PWR operating conditions.

- Deformable Ishii-Zuber drag force (independent of bubble diameter)
- $C_l = -0.03$ : negative constant lift coefficient
- No wall correction : unnecessary thanks to lift force  
→ Selected momentum closure terms are independent of bubble diameter

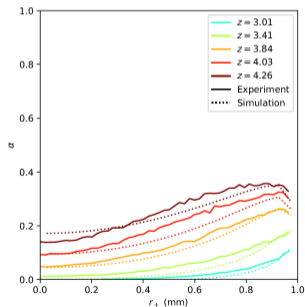


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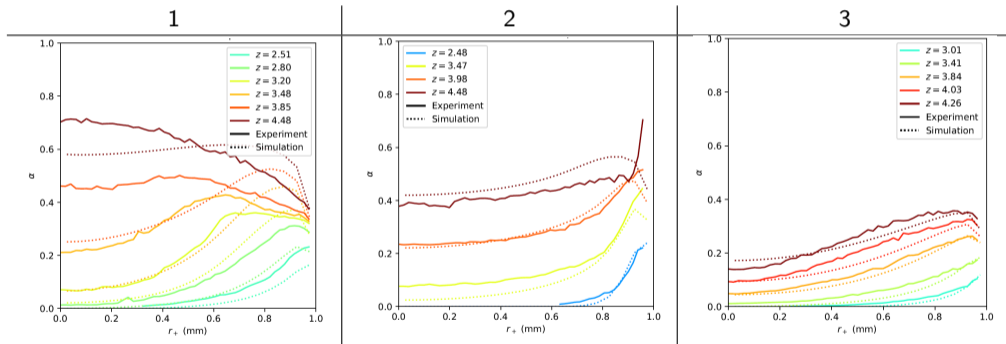
→ Selected momentum closure terms are independent of bubble diameter



*NB: the selected closures work on ~10 unpublished PWR-operating conditions*

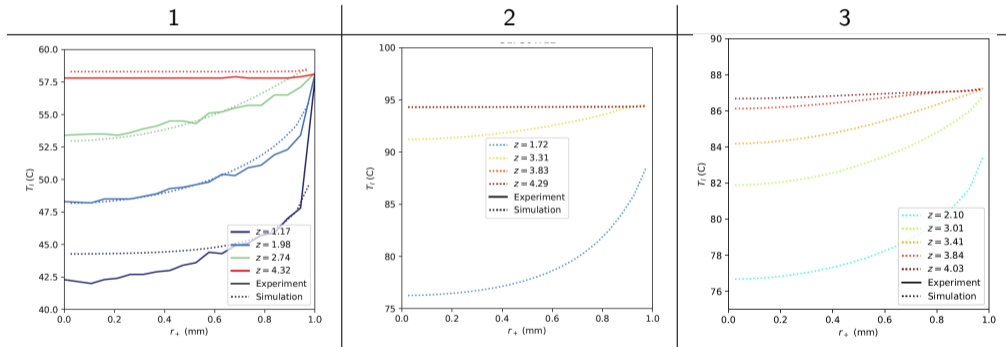
## 4. Boiling pipe flow in PWR similarity

Modifying the models to improve PWR in operation case (3) impairs the others



## 4. Boiling pipe flow in PWR similarity

The liquid is at saturation temperature at the wall at the top of the tube in all simulations



→ CHF criterion on evacuation of void fraction from the wall and not energy ?

## Conclusion

Take-home messages :

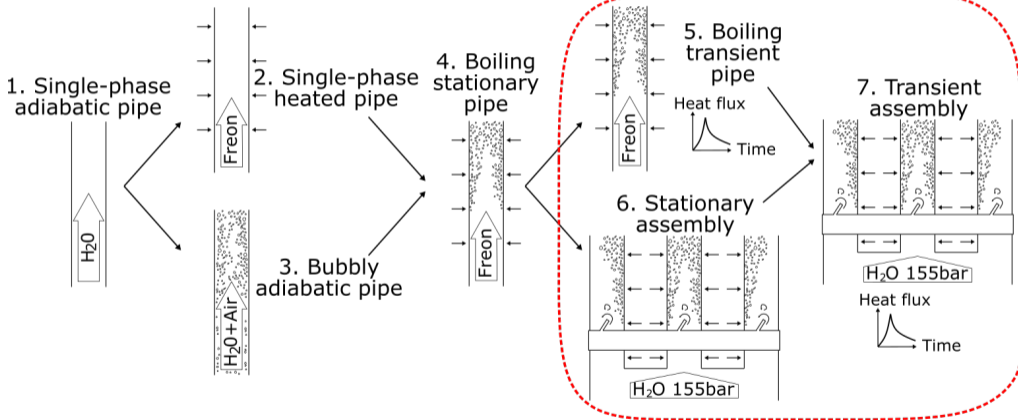
- We simulate boiling flows by enforcing the **experimental diameter**
- Atmospheric-pressure closure models are not adapted to **nuclear reactor-conditions**

Next steps :

- Finalize the choice of a set of **momentum and energy** closures that is adapted to reactor conditions
- Model the bubble diameter in reactor conditions
- Simulate the physical properties at the wall near the critical heat flux

# Conclusion

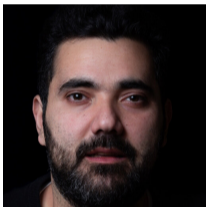
Third year or following PhD student ?



## TRUST and TrioCFD platforms

- <https://github.com/cea-trust-platform>
- <https://trio CFD.cea.fr/>
- <https://github.com/cea-trust-platform/TrioCFD-code>

## Thanks to



Elie Saikali



Yannick Gorsse



Antoine Gerschenfeld



Catherine Colin